



Comparison of Flow and Sedimentation Pattern for three Designs of Storm Water Tanks by Numerical Modelling

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- Objectives and goals
- Storm water tanks
- Requirements in Germany
- Compared storm water tanks
 - Dimensions
 - Hydraulic and particular conditions
- Results
 - Velocity distribution
 - Particle distribution
 - Sedimentation efficiency
- Conclusions



Pollution of surface waters:

- Particles in urban runoff
- Heavy metals mostly bounded at particles $< 60 \mu\text{m}$ (0.06 mm)

Treatment by sedimentation tanks

- about 30,000 storm water tanks in Germany
- investment volume 30 billion €
- efficiencies about and less than 30 %

Aim of investigation

- optimize tank design
 - flow pattern
 - sedimentation efficiency
- } different dimensions of tanks

- Sedimentation of particular loads in storm water
- Application in combined- and **separate sewer system**
 - combined sewer: e.g. combined sewer overflow tank
 - **separate system: e.g. storm water sedimentation tank**

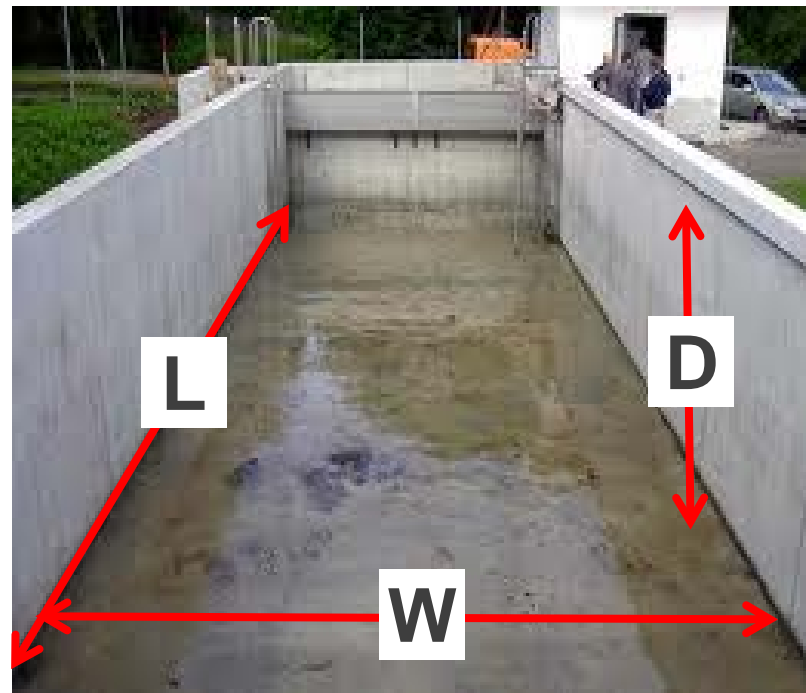
Relations

$$10 < L : D < 15$$

$$3 < L : W < 4,5$$

$$2 < W : D < 4$$

(according to German guidelines)

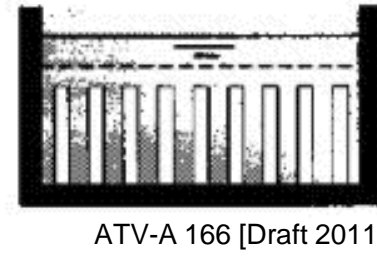
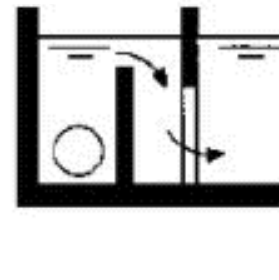
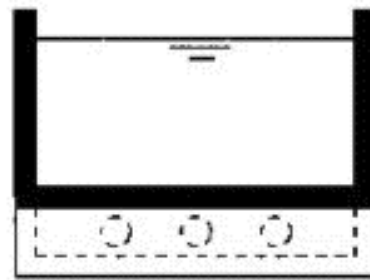
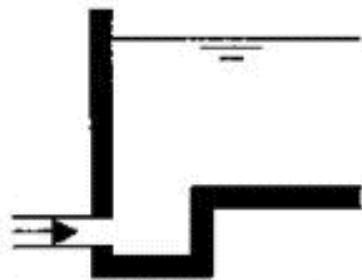
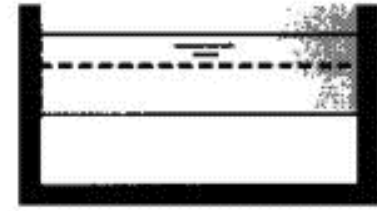
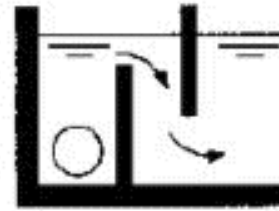
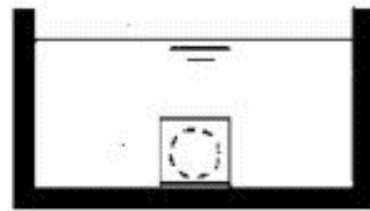
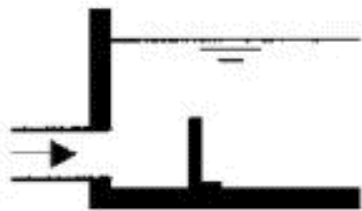
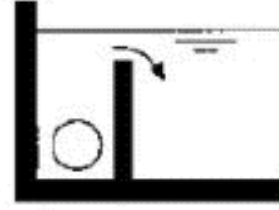
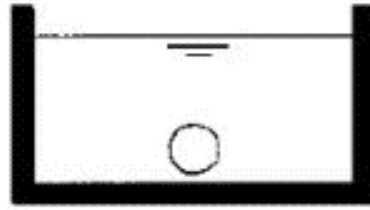
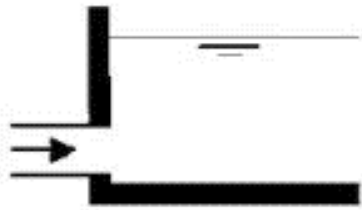


Requirements in Germany

Design of storm water sedimentation tanks



inlet requirements



ATV-A 166 [Draft 2011]

Requirements in Germany

Design of storm water sedimentation tanks



hydraulic requirements

mean horizontal velocity
(tank)

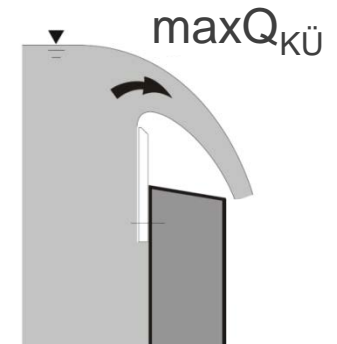
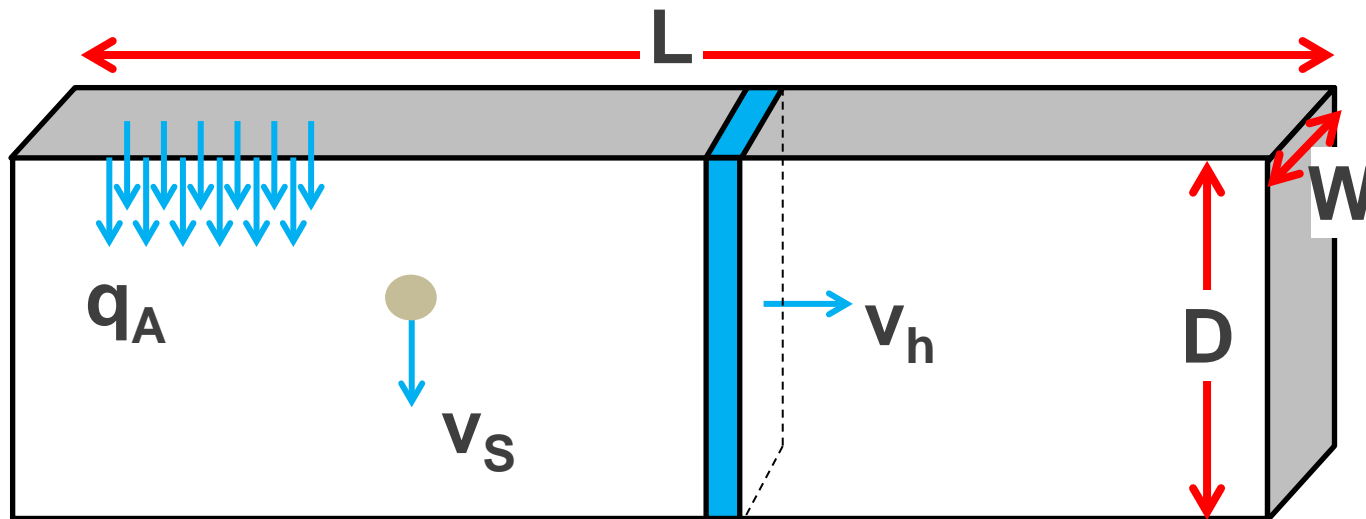
$$v_h = \frac{\max Q_{K\ddot{U}}}{W * D} \quad (\text{m/s})$$

surface flow rate
(mean vertical velocity)

$$q_A = \frac{\max Q_{K\ddot{U}} * 3.600}{W * L} \quad (\text{m/h})$$

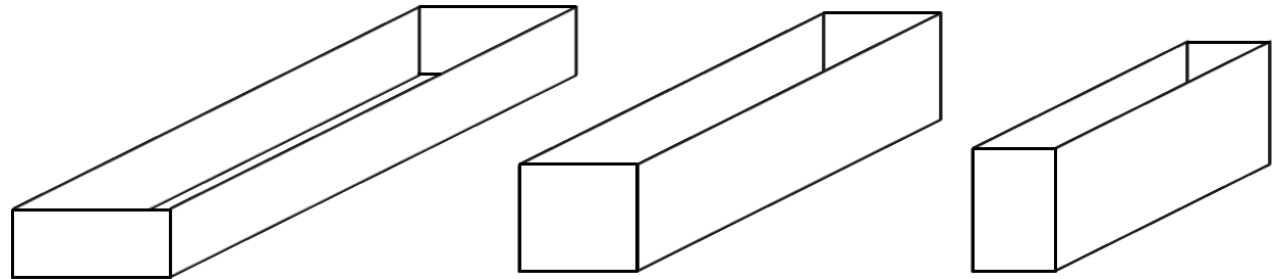
settling velocity
(STOKES)

$$v_s = \frac{1}{18} \rho' g d \frac{d}{v} \quad (\text{m/h})$$




Compared storm water sedimentation tanks

Tank relations

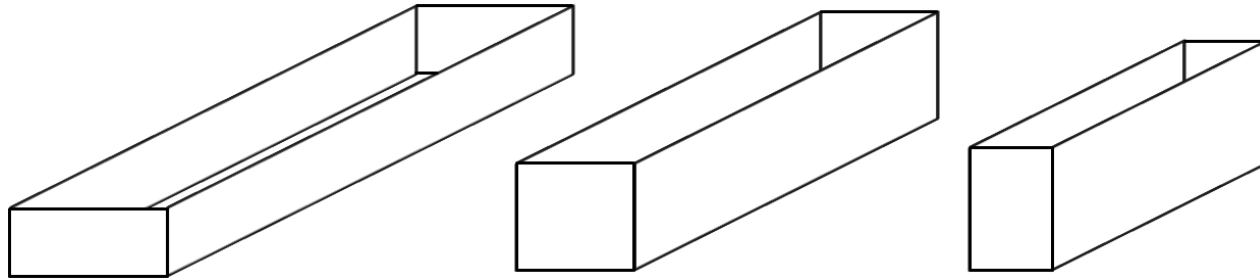


	Tank 1	Tank 2	Tank 3
Length L (m)	31,25	29,74	28,23
Width W (m)	8,00	7,14	6,27
Depth D (m)	2,00	2,36	2,82
L/D	15,6	12,6	10,0
L/W	3,9	4,2	4,5
W/D	4,0	3,0	2,2

 **Volume of each Tank: 500 m³**

Compared storm water sedimentation tanks

Hydraulic and particular conditions



Hydraulic boundary conditions

	Tank 1			Tank 2			Tank 3		
q_A (m/h)	2	6	10	2	6	10	2	6	10
v_h (m/s)	0.01	0.03	0.04	0.01	0.02	0.04	0.01	0.02	0.03

Properties of particles

Specific Density (kg/m ³)	1020				1460				2650			
v_s (m/h)	1	2.3	5	10	1	2.3	5	10	1	2.3	5	10
Diameter (μm)	181	275	405	573	38	58	85	120	20	30	45	64



Simulations by using FLUENT 13.0 CFD

- **boundary conditions:**
 - **inlet:** mass flow inlet
 - **outlet:** pressure outlet
 - **Wall-treatment:** no slip and standard wall functions
 - **roughness of the wall:** 5 mm
 - **Water surface:** symmetry plain
- **Solution method:** steady (*const. inflow*)
- **Turbulence model:** k- ϵ RNG modell
- **Sedimentation of solids:** uncoupled DPM (*Discrete Phase Model*)
- **Mesh size:** 600,000 cells (after a mesh study)



Limitations

- Resuspension based on the variability of the flow pattern cannot be modelled
- Shields does not apply for very small particles, since other effects like cohesion occur

Shields Relationship Vanoni [1975]

τ_{crit} critical shear stress [Pa]
 τ_0^* dimensionless shear stress
 β parameter

$$\tau_0^* = 0,22 \cdot \beta + 0,06 \cdot 10^{-7,7 \cdot \beta}$$

$$\beta = \left[\frac{\rho}{\mu} \cdot \sqrt{\left(\frac{(\rho_p - \rho)}{\rho} \right) \cdot g \cdot d^3} \right]^{-0,6}$$

Combination to an UDF
(User Defined
Function) (Vanoni after
Dufresne et. al. [2009])

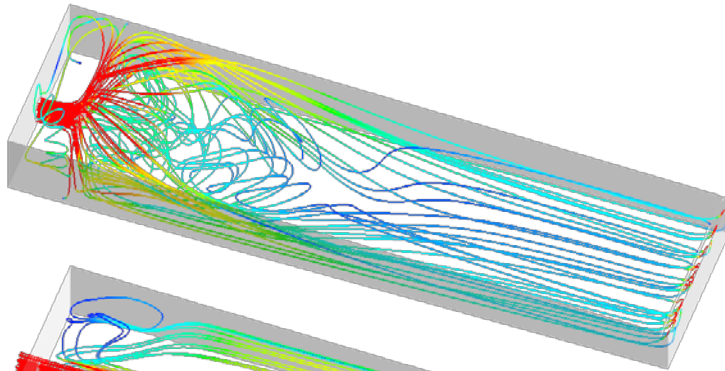
Velocity distribution

Streamlines

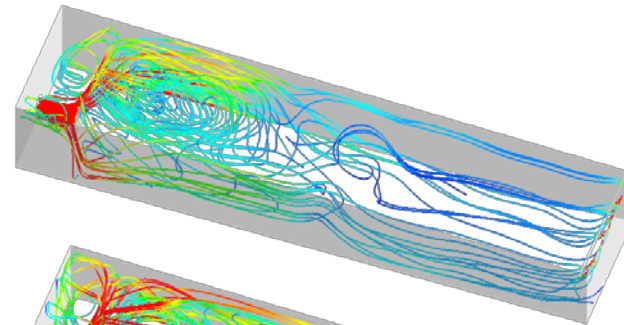


2 m/h

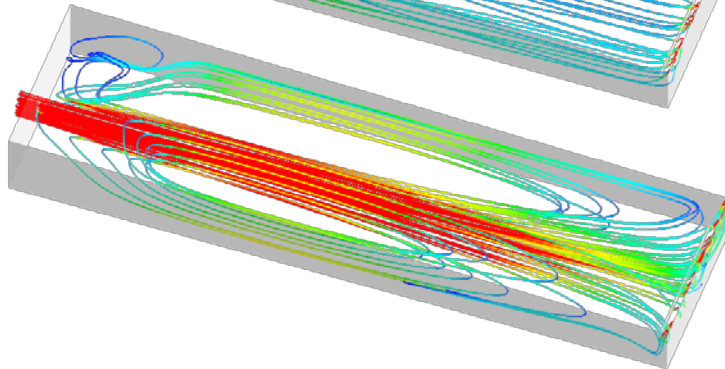
tank 1



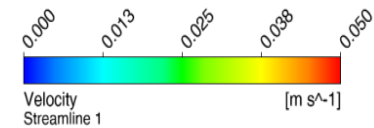
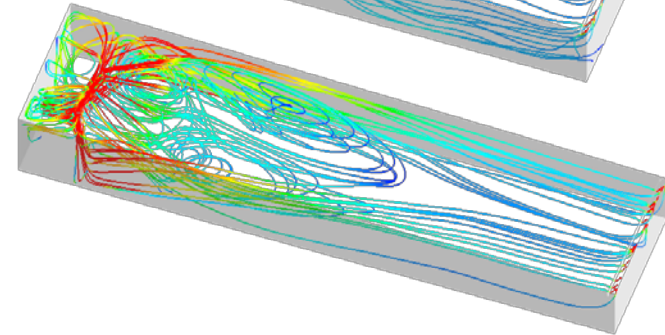
tank 3



tank 1a



tank 2

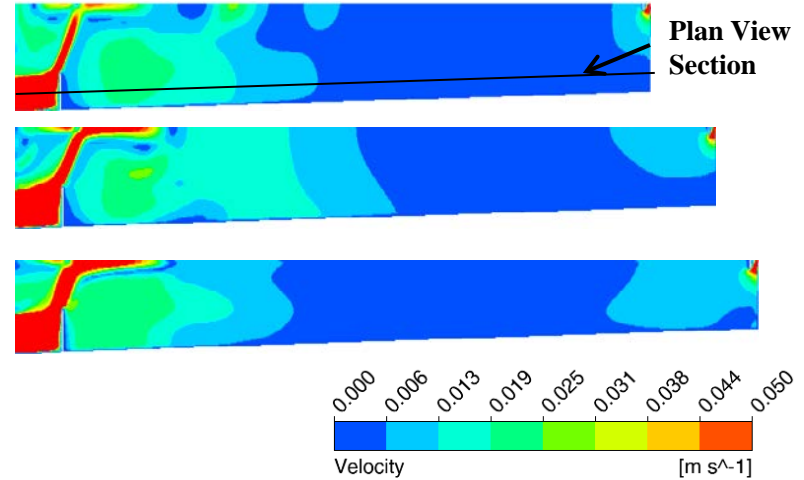
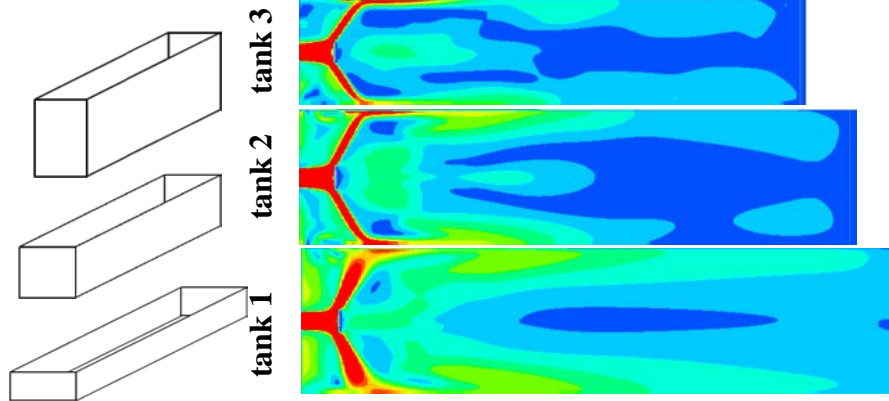


Velocity distribution

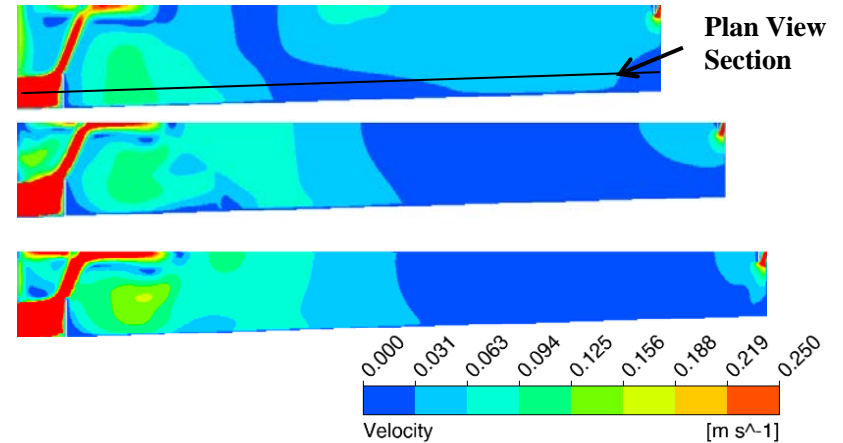
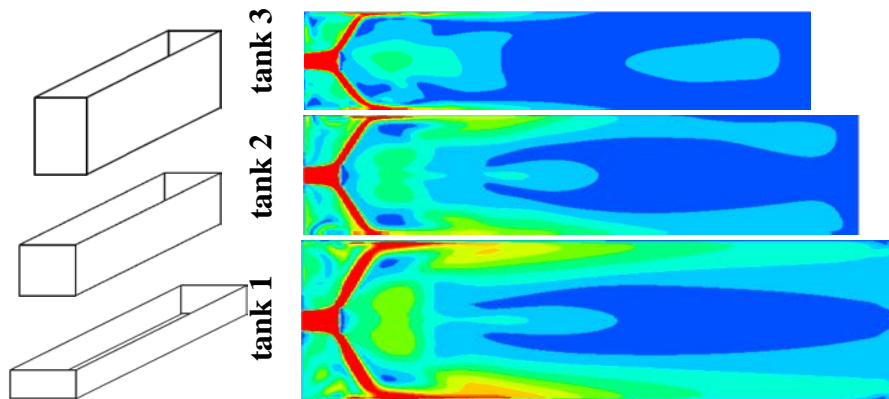
Velocity magnitude



2 m/h



10 m/h



Particle distribution

Bed shear stress

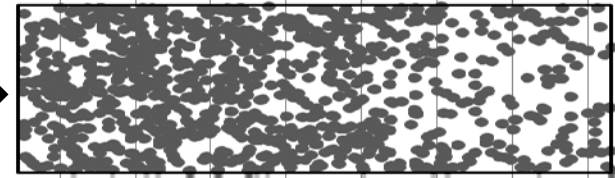


Density **1460 (kg/m³)**

v_s 2.3 (m/h)

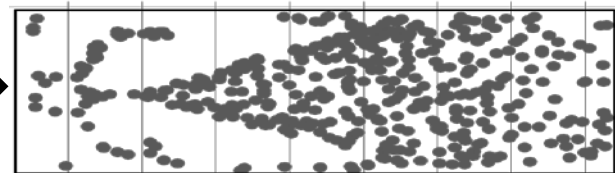
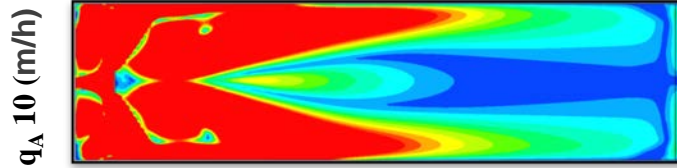
Ø 58 µm

Tank 1



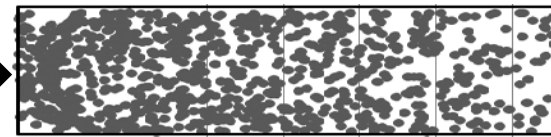
η

90 %

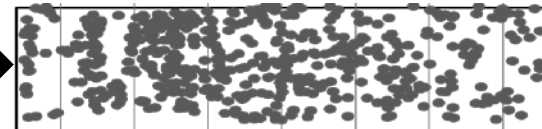
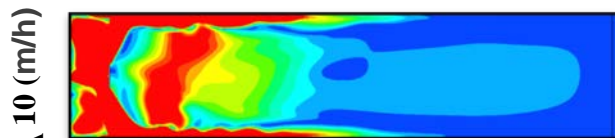


46 %

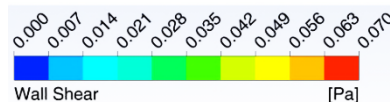
Tank 3



90 %



49 %



Particle distribution

Resuspension



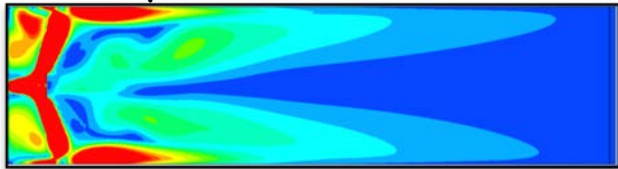
Density **1020 (kg/m³)**

v_s 2.3 (m/h)

Ø 275 µm

Tank 1

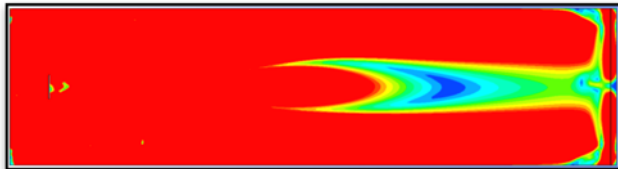
q_A 2 (m/h)



η

91 %

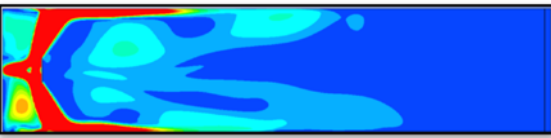
q_A 10 (m/h)



17 %

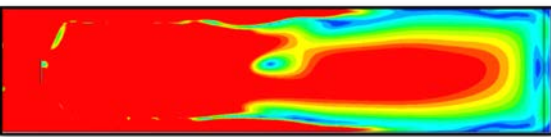
Tank 3

q_A 2 (m/h)



90 %

q_A 10 (m/h)



32 %

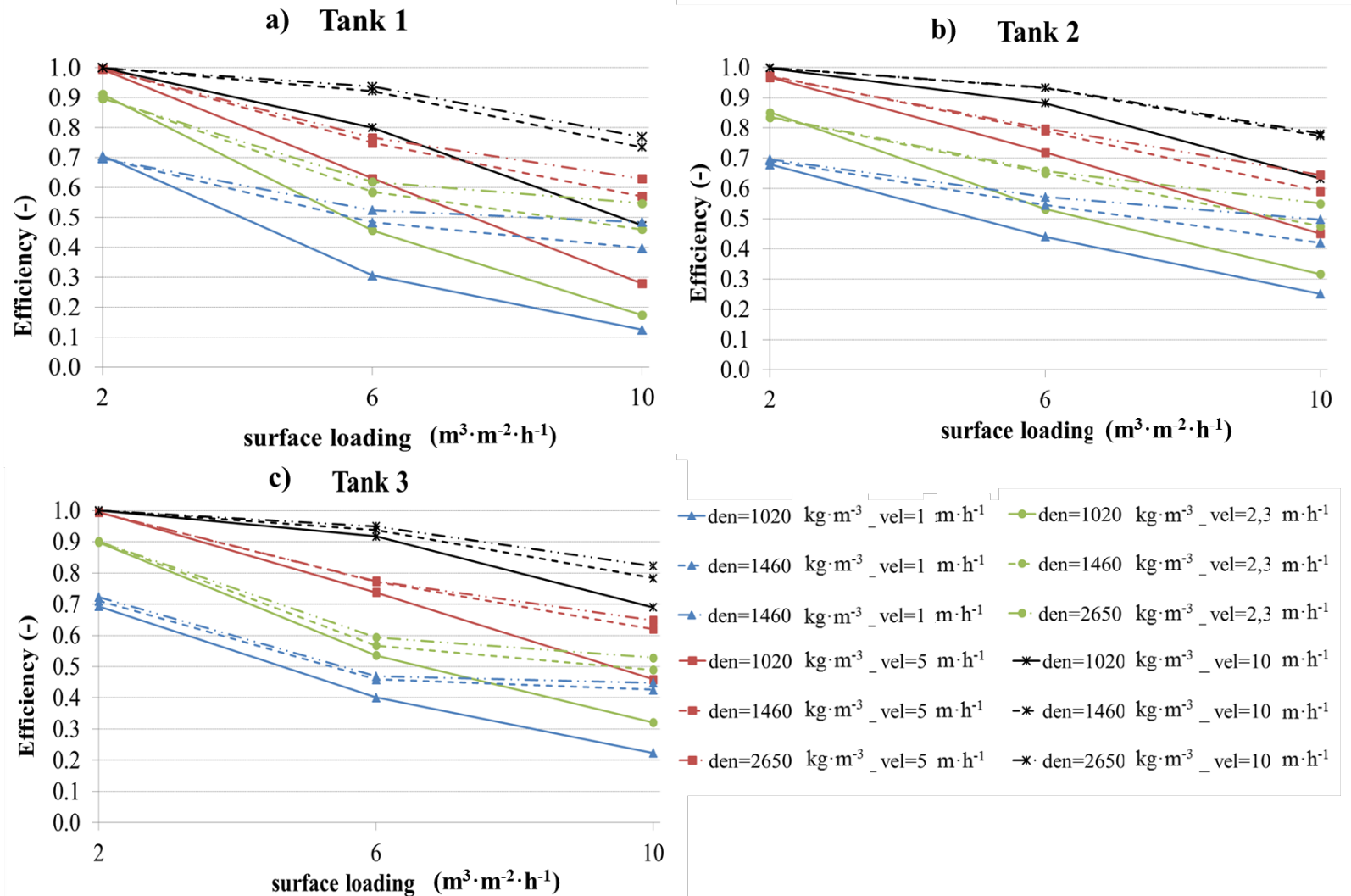
short hydraulic load



sediment gets resuspended



Overview of all simulation results





Low surface flow rate:

- efficiency is **independent** from geometry and density - similar for all tanks

High particle density:

- no differences in efficiency between high and low flow rates for all tanks

Low particle density:

- best sedimentation efficiency in **deep** tank- especially for higher surface flow rates



The deeper the tank the higher the sedimentation efficiency for organic matter



No effect on the efficiency, when there is low organic matter, by varying the dimensions in the ranges given by German standards