



Development of a semi-automated model identification and calibration tool for conceptual modelling of sewer systems

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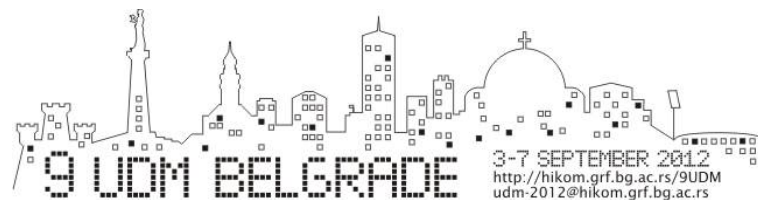
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Introduction

- Short computation time is often essential
- Current methods:
 - Physically based: de Saint-Venant equations
 - Conceptual: eg. Unit Hydrograph method, Muskingum routing
- Aim: development of a modelling approach which:
 - delivers accurate results for all types of flow
 - has very limited calculation times
 - allows for semi-automatic model structure identification and calibration
- Investigate:
 - Lumped conceptual modelling approach
 - Strong physical background
 - Calculate throughflow and overflow discharges

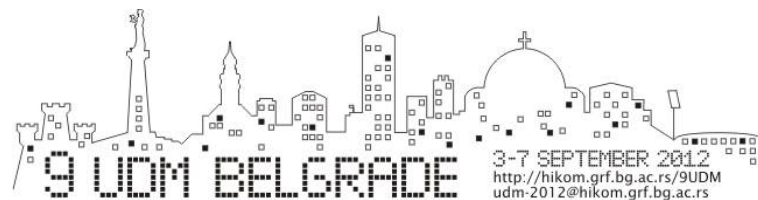


- Model presentation
 - Concept of the modelling approach
 - Characterisation of a sewer system
 - Transfer Function (TF) models
 - Automation of model structure identification and calibration
- Case Study
- Results
- Conclusions



Modelling approach

- Reservoir model
 - INFLOW: rainfall runoff, upstream systems, DWF, ...
 - OUTFLOW: throughflow and overflow
- Calibration and validation data: simulation results of a detailed hydrodynamic model (ic. InfoWorks CS)
- Research is limited to the hydraulic aspects



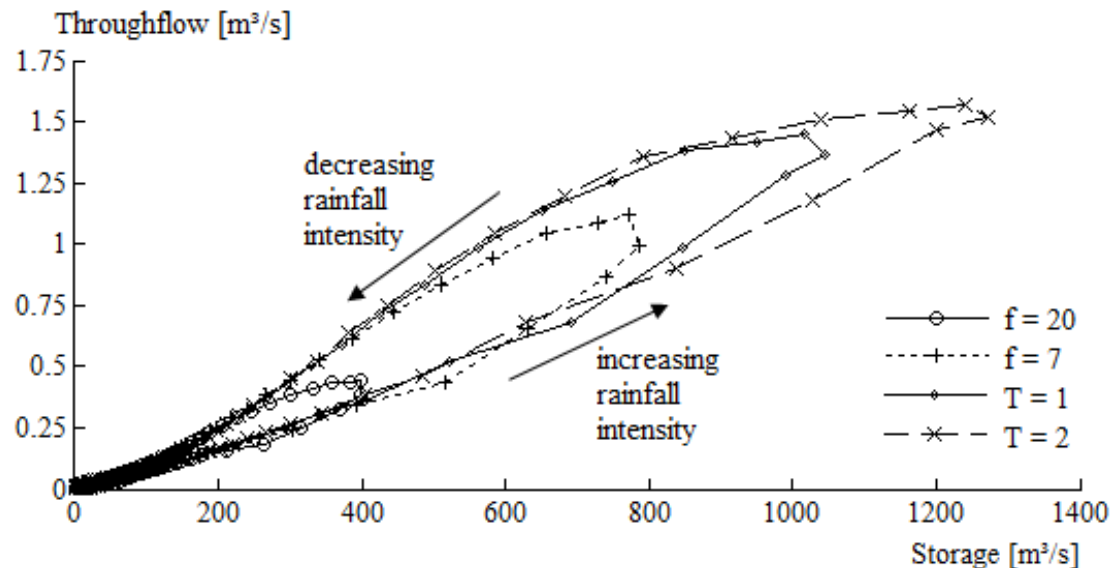
Sewer system characterisation (1)

a. Concentration time:

- Smoothing of the inflow hydrograph
- Done by averaging the runoff over the concentration time
- Approximated (constant) as the center of gravity difference between the rainfall input and total outgoing flow

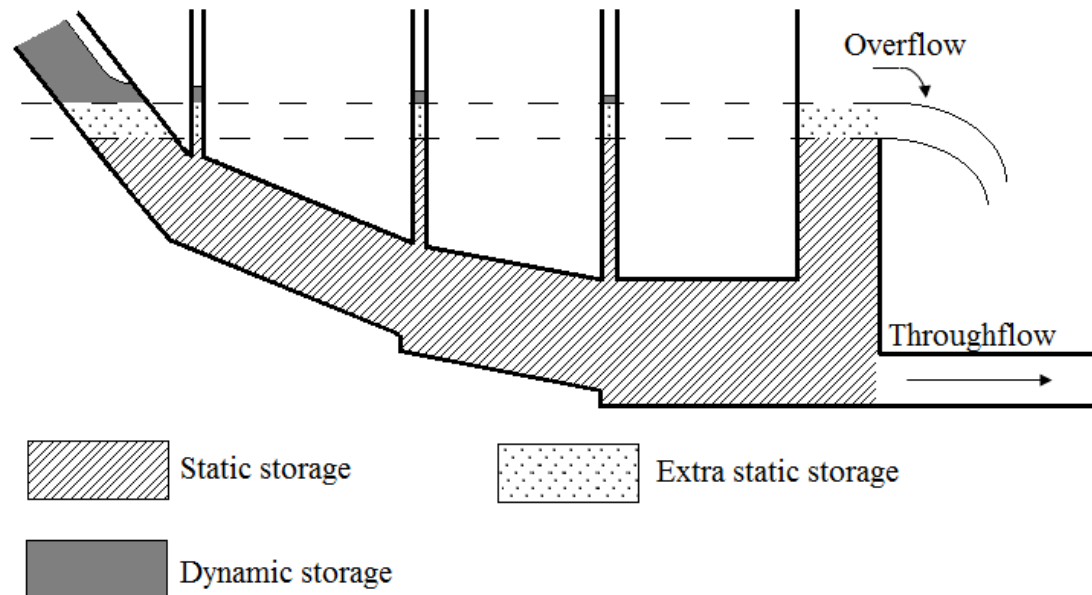
b. Storage/throughflow-relationships:

- Illustration: InfoWorks CS simulation results of a small fictitious gravity sewer system



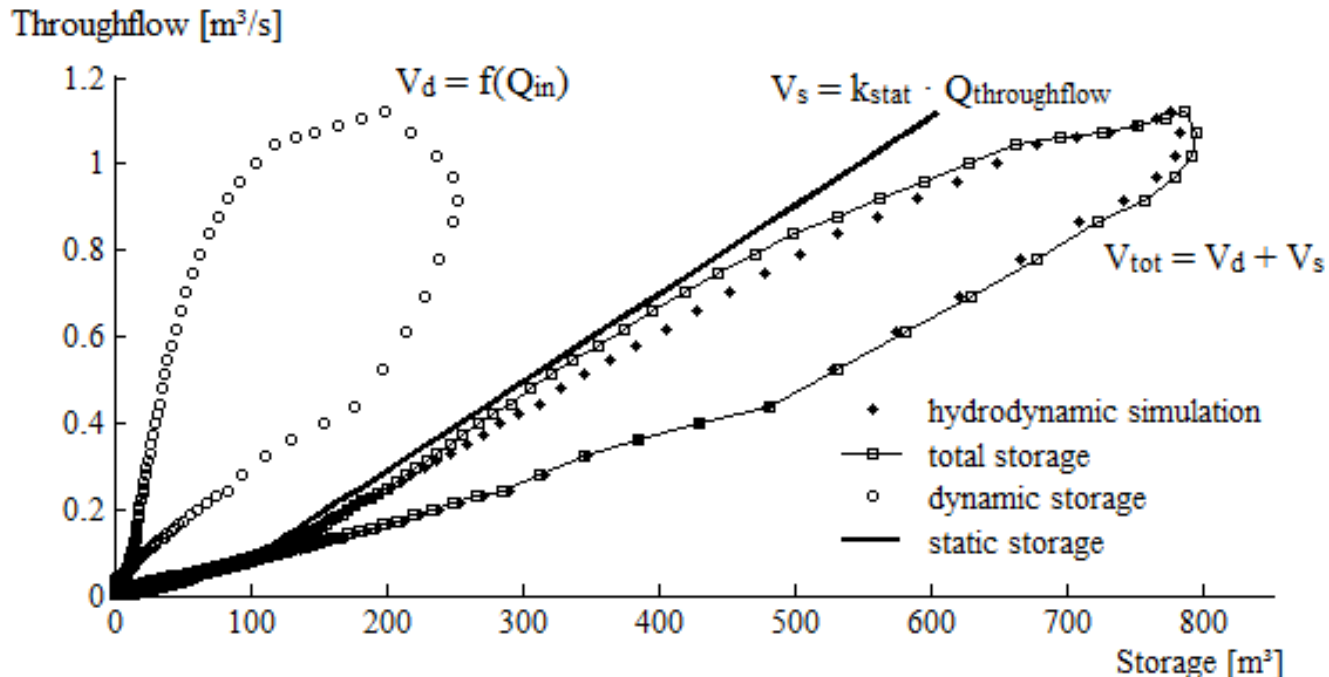
Sewer system characterisation (2)

- Approach: division of storage in several artificial components (Vaes, 1999):
 - Static storage
 - Dynamic storage
 - Extra static storage during overflow



Sewer system characterisation (3)

- Static storage: related to the throughflow
- Dynamic storage: related to the incoming flow



Transfer Function (TF) model (1)


- Use of TF's:
 - flexibility
 - suitable for semi-automatic model structure identification and calibration
- Chow (1988), Beven (2001):

$$Q_t = \frac{b_0 + b_1 z^{-1} + \dots + b_m z^{-m}}{1 - a_1 z^{-1} - \dots - a_n z^{-n}} z^{-\delta} I_t \quad \text{with } z^1 Q_t = Q_{t-1} \quad (\text{eq. 1})$$

$$S_t = S_{dyn,t} + S_{stat,t} \quad (\text{eq. 2})$$

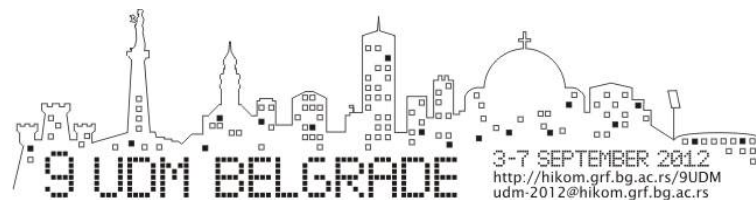
$$S_{dyn,t} = r_d \cdot I_t \quad (\text{eq. 3})$$

$$S_{stat,t} = r_s \cdot Q_t \quad (\text{eq. 4})$$

+ continuity equation 
$$Q_t \cdot \left(1 - \left(1 - \frac{\Delta t}{r_s} \right) \cdot z^{-1} \right) = I_t \cdot \left(-\frac{r_d}{r_s} + \left(\frac{r_d + \Delta t}{r_s} \right) \cdot z^{-1} \right) \quad (\text{eq. 5})$$

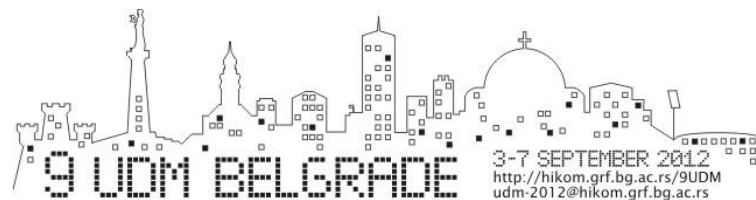
Transfer Function (TF) model (2)

- More complex relationships for S_{stat} en S_{dyn} possible:
 - Dependence on different time steps: eg. $S_{\text{dyn}} \sim I_t$ and I_{t-1}
 - Piecewise linear relationships
- Several approaches:
 1. Analytical solution (eq. 5) \rightarrow “CM method 1”
 2. Uncoupled static and dynamic volume \rightarrow “CM method 2”:
 - Static Volume \sim Outflow (piecewise linear relationships)
 - Dynamic Volume = an arrangement of linear reservoirs depending on the incoming flow (TF)



Automation

- MATLAB/Simulink[®] tool with GUI
- Inputs: simulation results (incoming flow, throughflow and overflow) and timestep
- TF calibration by means of the Captain Toolbox (Young et al., 2007):
 - Identification: Cross-correlation function (Box and Jenkins, 1970) and various statistical criteria such as YIC (Young, 1984).
 - Parameter estimation: Refined Instrumental Variable (Pedregal, 2007).
- Self chosen values of r_s and r_d (cf. eq. 3 and 4)



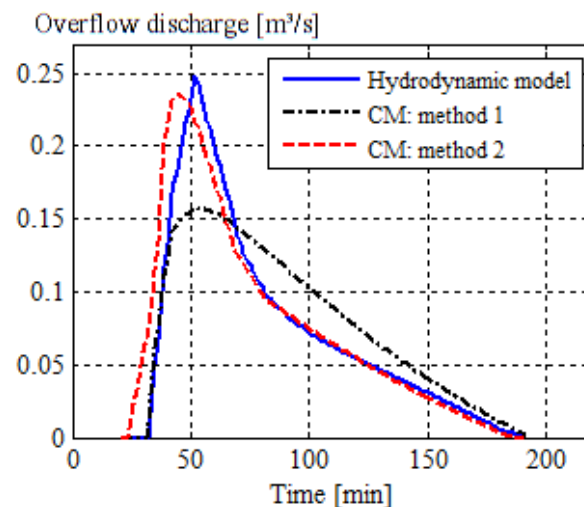
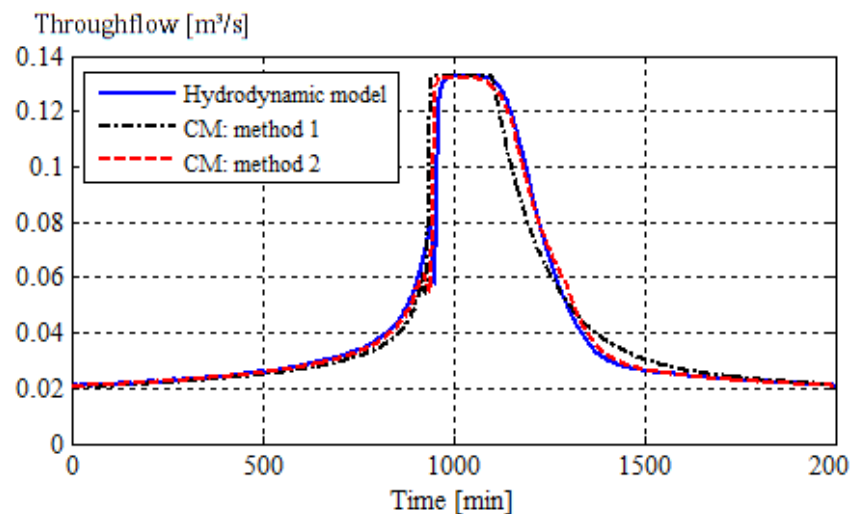
Case Study

- Sewer system of the city of Geel, Grote Nete Catchment, Flanders, Belgium.
- Detailed InfoWorks CS (IWCS) model (provided by the water company Aquafin)
- Characteristics of the considered subsystem:
 - Reduced area of 12.33 ha
 - Population equivalent of 430
 - 3 CSO's
- Rainfall used for simulations in IWCS:
 - Composite storms with frequencies ranging from 20 ('f20') to 1 ('f1') per year, and return periods from 2 ('T2') to 20 years ('T20') with a timestep of 10 minutes and duration of 48 hours.
 - Long term time series of rainfall measurements from 13 sept. 2001 – 11 jan. 2010 with a 15-minute timestep.



Results: composite storms

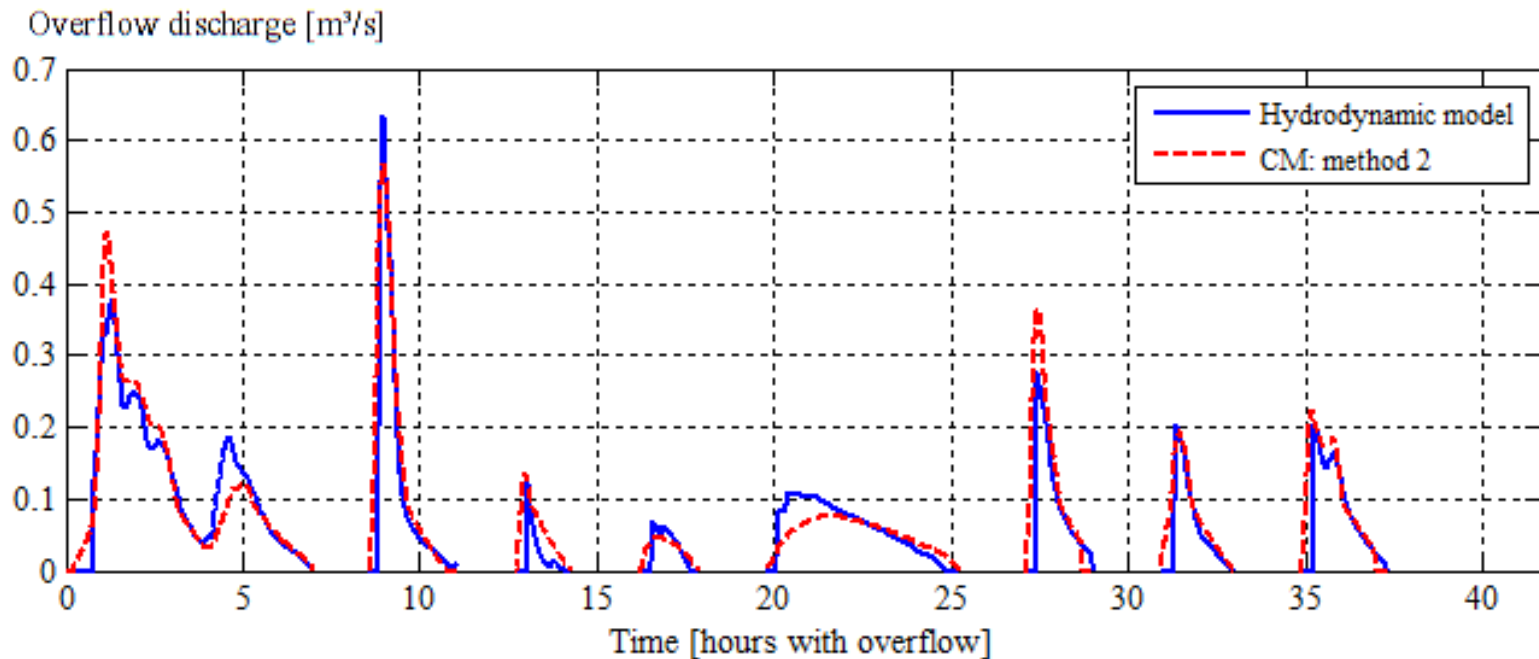
- Hydrographs of the throughflow and cumulated CSO discharges for the composite storm T2



<i>(NSE values)</i>		f20	f10	f7	f1	T2	T5	T10	T20
Throughflow	CM1	0.91	0.96	0.96	0.97	0.95	0.93	0.93	0.92
	CM2	0.97	0.98	0.99	0.99	0.98	0.97	0.97	0.95
Cumulated CSO discharge	CM1	n.a.	n.a.	n.a.	0.86	0.92	0.77	0.66	0.60
	CM2	n.a.	n.a.	n.a.	0.78	0.94	0.96	0.97	0.97

Results: long term simulation

- Long term simulation (8 years)



- Calculation time < 3 minutes (1 minute time step)

Conclusions

- Current (conceptual) models:
 - Critical calculation time
 - Often lack accuracy in predicting (CSO) discharges
 - Calibration process is time-consuming
- Presented modelling approach:
 - Physical approach: division in several storage components
 - Use of Transfer Functions led to two methodologies
 - Calibration semi-automatic process
- Case study (InfoWorks CS model):
 - Composite storms and long term simulations used
 - Significant shorter calculation time
 - Accurate and stable results



References

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